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指标函数终端自由和受函数约束 的分数阶系统的最优控制

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摘要: 将求解整数阶系统最优控制的方法和步骤拓展到分数阶系统的最优控制中, 对由 Caputo 定义的分阶微分方程描述的分数阶系统提出了求解性能指标函数在始端固定的条件下, 终端时间固定而终端状态自由和始端固定、终端时间固定而终端状态受函数约束的最优控制的状态方程、伴随方程、控制方程、横截条件和终端约束方程, 并给予了证明。

关键词: 分数阶系统; 最优控制; 性能指标函数

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0 引言

分数阶微积分是研究任意阶次微分和积分的理论, 分数阶系统是指由分数阶微分方程描述的系统。理论和实践证明, 用分数阶微分方程来描述实际中的某些系统更为准确恰当, 如热力学系统、柔性系统、黏性系统^[1]等。

目前对于分数阶控制系统的研究已经有了一些成果, 如在其数值实现、能控能观性分析、稳定性分析等方面。但在分数阶系统的最优控制方面, 国内外的研究还处于起步阶段。Agrawa 证明了 Riemann-Liouville 定义下的左边分数阶微分和右边分数阶微分的一种变分形式, 解决了指定边界条件分数阶函数最小化问题和有约束条件的指定边界问题的函数最小化问题^[2-3]。Frederico 等发展了 Agrawa 的理论, 提出了在 Caputo 定义下的分数阶最优控制的变分实现问题^[4]。Christophe 等介绍了一种新的近似解决分数阶最优控制问题的基于系统冲击响应的奇异值分解的有理近似的方法^[5-6]。

笔者在给出分数阶系统最优控制的定义的基础上, 求解了在 Caputo 定义下的分数阶系统指标函数终端自由的最优控制问题和系统终端时间 t_f 固定, 终端受函数约束的最优控制, 给出了相应的

定理及其证明。

1 分数阶微积分及其性质

分数阶微积分是研究任意阶次微分和积分的理论, 它是整数阶微积分的自然延伸。用符号 I_a^α 和 ${}_aD_t^\alpha$ 分别表示分数阶积分和微分, 其中 α 和 t 为积分的上下限, α 为任意实数。

笔者用到的分数阶积分和微分的定义和主要性质如下^[2-4]:

(1) Riemann-Liouville 积分定义

$$I_a^\alpha f(t) = \frac{1}{\Gamma(\alpha)} \int_a^t (t-\tau)^{\alpha-1} f(\tau) d\tau, m-1 < \alpha < m, m \in N; \quad (1)$$

(2) 左边 Riemann-Liouville 微分定义

$${}_aD_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \left(\frac{d}{dt} \right)^m \int_a^t \left[\frac{f(\tau)}{(t-\tau)^{\alpha-m+1}} \right] d\tau, m-1 < \alpha < m, m \in N; \quad (2)$$

(3) 右边 Riemann-Liouville 微分定义

$${}_bD_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \left(-\frac{d}{dt} \right)^m \int_t^b [f(\tau)(\tau-t)^{\alpha-m-1}] d\tau, m-1 < \alpha < m, m \in N; \quad (3)$$

(4) 左边 Caputo 微分定义

$${}_a^c D_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \int_a^t \frac{f''(\tau)}{(t-\tau)^{\alpha-m+1}} d\tau, m-1 < \alpha < m, m \in N; \quad (4)$$

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(5) 右边 Caputo 微分定义

$${}_a^C D_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \int_a^t \frac{(-1)^m f^{(m)}(\tau)}{(\tau-t)^{\alpha-m+1}} d\tau, \quad m-1 < \alpha < m, m \in N. \quad (5)$$

(6) 分数阶微积分的分部积分

$$\int_a^b g(x) {}_a^C D_x^\alpha f(x) dx = \int_a^b f(x) {}_a D_x^\alpha g(x) dx + \sum_{j=0}^{n-1} [(-1)^{n-j} D_x^{\alpha+j-n} g(x) \cdot {}_a D_x^{\alpha-1-j} f(x)]_a^b. \quad (6)$$

$$\int_a^b g(x) {}_a^C D_x^\alpha f(x) dx = \int_a^b f(x) {}_a D_x^\alpha g(x) dx + \sum_{j=0}^{n-1} [{}_a D_x^{\alpha+j-n} g(x) \cdot {}_a D_x^{\alpha-1-j} f(x)]_a^b. \quad (7)$$

特别地,当 $0 < \alpha < 1$ 时,有

$$\int_a^b g(x) {}_a^C D_x^\alpha f(x) dx = \int_a^b f(x) {}_a D_x^\alpha g(x) dx - [{}_a I_x^{1-\alpha} g(x) \cdot f(x)]_a^b, \quad (8)$$

$$\int_a^b g(x) {}_a^C D_x^\alpha f(x) dx = \int_a^b f(x) {}_a D_x^\alpha g(x) dx + [{}_a I_x^{1-\alpha} g(x) \cdot f(x)]_a^b. \quad (9)$$

2 分数阶系统最优控制的求解

笔者主要研究基于 Caputo 定义的分数阶微分方程所描述的系统. 设分数阶系统形式如下:

$${}_a^C D_t^\alpha x(t) = f[x(t), u(t), t], \quad (10)$$

式中: $x(t)$ 为 n 维状态变量; $u(t)$ 为 r 维控制变量; $f[\cdot]$ 为 n 维向量函数. 为了求解简单, 令 $0 < \alpha < 1$. 系统的指标泛函为:

$$J = \Phi(t_f, x(t_f)) + \int_{t_0}^{t_f} L[x(t), u(t), t] dt. \quad (11)$$

式中: t_f 和 $x(t_f)$ 分别表示终端时刻和终端状态.

定义1 分数阶系统(10)的最优控制, 就是确定最优控制向量 $u^*(t)$ 和最优曲线 $x^*(t)$, 使系统(10)由初始状态转移到终端状态, 并使给定的指标泛函式(11)达到极值.

2.1 指标泛函始端固定、终端状态自由的分数阶系统的最优控制

定理1 设分数阶系统的状态方程为

$${}_a^C D_t^\alpha x(t) = f[x(t), u(t), t],$$

系统始端满足: $x(t_0) = x_0$, 终端时间 t_f 固定, $x(t_f)$ 自由. 则把状态 $x(t)$ 自始端 $x(t_0) = x_0$, 转移到 $x(t_f)$, 并使分数阶系统的性能指标泛函

$$J = \Phi(t_f, x(t_f)) + \int_{t_0}^{t_f} L[x(t), u(t), t] dt,$$

取极值, 以实现最优控制的必要条件是

(1) 最优控制曲线 $x^*(t)$ 和最优伴随向量 $\lambda^*(t)$ 满足状态方程和伴随方程:

$${}_a^C D_t^\alpha x(t) = f[x(t), u(t), t],$$

$$\frac{\partial H}{\partial x(t)} = {}_t D_{t_f}^\alpha \lambda^T,$$

其中: $H = L + \lambda^T f$, 式中 H 为哈密顿函数, 它是 $x(t)$, $u(t)$, $\lambda(t)$ 和 t 的函数.

(2) 最优控制向量 $u^*(t)$ 满足控制方程:

$$\partial H / \partial u = 0.$$

(3) 横截条件:

$$\left. \frac{\partial \Phi}{\partial x} \right|_{t=t_f} = 0, x(t_0) = x_0, \lambda(t_f) = 0.$$

证明 由描述系统的分数阶微分方程可知:

$$J = \Phi(t_f, x(t_f)) + \int_{t_0}^{t_f} [H - \lambda^T {}_a^C D_t^\alpha x(t)] dt, \quad (12)$$

其中 H 为 Hamilton 函数, $H = L + \lambda^T f$.

对式(12)求变分得:

$$\delta J = \left(\frac{\partial \Phi}{\partial x} \right)^T \delta x \Big|_{t=t_f} + \int_{t_0}^{t_f} \left[\left(\frac{\partial H}{\partial u} \right)^T \delta u + \left(\frac{\partial H}{\partial x} \right)^T \delta x - \lambda^T \delta({}_a^C D_t^\alpha x(t)) \right] dt. \quad (13)$$

根据分数阶微积分的分部积分式(6), 可得:

$$\int_{t_0}^{t_f} \lambda^T \delta({}_a^C D_t^\alpha x(t)) dt = \int_{t_0}^{t_f} \delta x {}_t D_{t_f}^\alpha \lambda^T dt. \quad (14)$$

在 $\delta x(t_0) = 0$ 或者 $\lambda(t_0) = 0$, $\delta x(t_f) = 0$ 或者 $\lambda(t_f) = 0$ 的条件下成立. 由于 $x(t_0) = x_0$, 所以有 $\delta x(t_0) = 0$. 由于 $x(t_f)$ 自由, 所以令 $\lambda(t_f) = 0$ 即可满足.

将式(14)代入式(13)可得:

$$\delta J = \left(\frac{\partial \Phi}{\partial x} \right)^T \Big|_{t=t_f} - {}_{t_0} I_{t_f}^{1-\alpha} \lambda^T(t) \delta x \Big|_{t=t_f} + \int_{t_0}^{t_f} \left[\left(\frac{\partial H}{\partial u} \right)^T \delta u + \left(\frac{\partial H}{\partial x} \right)^T \delta x - ({}_t D_{t_f}^\alpha \lambda^T(t)) \delta x \right] dt. \quad (15)$$

要使泛函取得极值, 必有 $\delta J = 0$. 由此可得:

$$\text{状态方程 } {}_a^C D_t^\alpha x(t) = f[x(t), u(t), t]$$

$$\text{控制方程 } \partial H / \partial u = 0$$

$$\text{伴随方程 } \partial H / \partial x(t) = {}_t D_{t_f}^\alpha \lambda^T$$

$$\text{横截条件 } \partial \Phi / \partial x \Big|_{t=t_f} = 0$$

$$x(t_0) = x_0$$

$$\lambda(t_f) = 0$$

2.2 指标泛函始端固定、终端受函数约束的分数阶系统的最优控制

定理2 设分数阶系统的状态方程为:

$${}_a^C D_t^\alpha x(t) = f[x(t), u(t), t].$$

式中: $x(t)$ 为 n 维状态变量; $u(t)$ 为 r 维控制变量; $f[\cdot]$ 为 n 维向量函数. 为了求解简单, 令 $0 < \alpha < 1$.

系统始端状态满足: $x(t_0) = x_0$.

系统终端 t_f 固定, 终端状态 $x(t_f)$ 受下式约束

$$N_1[x(t_f), t_f] = 0. \quad (16)$$

式中: $N_1 = [N_{11}, N_{12}, \dots, N_{1m}]^T$. 则把状态 $x(t)$ 自始端 $x(t_0) = x_0$, 转移到 $x(t_f)$, 并使分数阶系统的性能指标泛函

$$J = \Phi(t_f, x(t_f)) + \int_{t_0}^{t_f} L[x(t), u(t), t] dt$$

取极值, 以实现最优控制的必要条件是:

(1) 最优控制曲线 $x^*(t)$ 和最优伴随向量 $\lambda^*(t)$ 满足状态方程和伴随方程

$${}_0^C D_t^\alpha x(t) = f[x(t), u(t), t],$$

$${}_0^C D_t^\alpha \lambda = \frac{\partial H}{\partial x};$$

(2) 最优控制向量 $u^*(t)$ 满足控制方程

$$\partial H / \partial u = 0;$$

(3) 横截条件

$$\left(\frac{\partial \Phi}{\partial x} + \left(\frac{\partial N_1^T}{\partial x} \right) \nu \right) \Big|_{t=t_f} = {}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \Big|_{t=t_f},$$

$$x(t_0) = x_0;$$

(4) 终端约束条件

$$N_1[x(t_f), t_f] = 0.$$

证明 现在存在两个约束条件, 即状态方程和终端约束方程. 为解决约束引入两个拉格朗日乘子向量 λ 和 ν . 即

$\mu = [\mu_1, \mu_2, \dots, \mu_n]^T, \nu = [\nu_1, \nu_2, \dots, \nu_m]^T$. 将式(17)与式(12)的泛函相联系, 于是有

$$J = \Phi(t_f, x(t_f)) + \nu^T N_1[x(t_f), t_f] + \int_{t_0}^{t_f} [H - \mu^T {}_0^C D_t^\alpha x(t)] dt. \quad (17)$$

其中 H 为 Hamilton 函数, $H = L + \lambda^T f$.

令 $\Phi_1[x(t_f), t_f] = \Phi(t_f, x(t_f)) + \nu^T N_1[x(t_f), t_f]$, 则有:

$$J = \Phi_1(t_f, x(t_f)) + \int_{t_0}^{t_f} [H - \lambda^T {}_0^C D_t^\alpha x(t)] dt. \quad (18)$$

根据分数阶微积分的分部积分的性质(6)可得:

$$\int_{t_0}^{t_f} \lambda^T {}_0^C D_t^\alpha x(t) dt = \int_{t_0}^{t_f} x(t) {}_0^C D_t^\alpha \lambda^T(t) dt + [{}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \cdot x(t)]_{t_0}^{t_f}. \quad (19)$$

将式(19)代入式(18)得:

$$\begin{aligned} J &= \Phi_1(t_f, x(t_f)) + \int_{t_0}^{t_f} [H - \lambda^T {}_0^C D_t^\alpha x(t)] dt \\ &= \Phi_1(t_f, x(t_f)) + \int_{t_0}^{t_f} [H - x(t) {}_0^C D_t^\alpha \lambda^T(t)] dt - \\ &\quad [{}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \cdot x(t)]_{t_0}^{t_f}. \end{aligned}$$

J 的一次变分为:

$$\delta J = \left(\frac{\partial \Phi_1}{\partial x} \right)^T \delta x \Big|_{t=t_f} + \int_{t_0}^{t_f} \left[\left(\frac{\partial H}{\partial u} \right)^T \delta u + \left(\frac{\partial H}{\partial x} \right)^T \delta x - \left({}_0^C D_t^\alpha \lambda^T(t) \right) \delta x \right] dt - \left[{}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \cdot \delta x \right]_{t_0}^{t_f}. \quad (20)$$

由于 $x(t_0)$ 固定, 所以 $\delta x(t_0) = 0$. 式(21)可以写为:

$$\delta J = \left(\left(\frac{\partial \Phi_1}{\partial x} \right)^T - {}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \right) \delta x \Big|_{t=t_f} + \int_{t_0}^{t_f} \left[\left(\frac{\partial H}{\partial u} \right)^T \delta u + \left(\frac{\partial H}{\partial x} \right)^T \delta x - \left({}_0^C D_t^\alpha \lambda^T(t) \right) \delta x \right] dt. \quad (21)$$

泛函极值存在的必要条件为 $\delta J = 0$, 由式(21)可得泛函存在极值的必要条件为

状态方程 ${}_0^C D_t^\alpha x(t) = f[x(t), u(t), t]$

伴随方程 ${}_0^C D_t^\alpha \lambda = \partial H / \partial x$

控制方程 $\partial H / \partial u = 0$

横截条件

$$\left(\frac{\partial \Phi}{\partial x} + \left(\frac{\partial N_1^T}{\partial x} \right) \nu \right) \Big|_{t=t_f} = {}_0^C I_{t_f}^{1-\alpha} \lambda^T(t) \Big|_{t=t_f}$$

$$x(t_0) = x_0$$

终端约束 $N_1[x(t_f), t_f] = 0$.

3 结论

笔者将求解整数阶系统最优控制的变分方法拓展到分数阶系统的最优控制问题中, 研究了基于 Caputo 定义的分数阶微分方程描述的系统的始端固定情况下, 终端时刻固定、终端状态自由和终端时刻固定、终端状态受函数约束的最优控制, 推导并得出了相应的状态方程、伴随方程、控制方程.

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Optimal Control of Fractional-Order System with Freedom End-Point or Function Constrained End-Point

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Abstract: The method of solving the optimal control problem for integer-order systems is extended into fractional-order in this paper. The optimal control of the systems described by Caputo's fractional-order differential equation is investigated. The state equation, concomitant equation, control equation, transversality conditions and terminal constraint equations of optimal control for fractional-order system with fixed terminal time, free terminal state and fixed terminal time function constrained end-point is proposed and proved exactly in the paper.

Key words: fractional-order system; optimal control; performance index function

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Research on Complete Compensation to Dynamic Characteristic of Temperature Sensor and Design of Compensating Circuit

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Abstract: The first-order system model and second-order system model for dynamic characteristic of temperature sensor are analysed. The second-order system is not a underdamping system and that there are similarity and intercommunity between the step responses of the two systems are pointed out, and then that the dynamic models of temperature sensor can be unified simplified as the first-order system model is put forward. The transfer function of compensating circuit which can make a first-order system to be compensated as a perfect all-pass system is derived. The active filter circuit which can realize the transfer function is designed, and the design formulas for calculating the circuit element parameters by thermal time constant of temperature sensor are given out. That the output voltage of signal conversion circuit are linear and proportionate to the sensor's temperature, and that compensating circuit and signal conversion circuit have sufficiently wide pass band, are pointed out as the two necessary conditions realizing complete compensation to dynamic characteristic of temperature sensor using hardware.

Key words: temperature sensor; dynamic measurement; dynamic error compensation; circuit design