

负性胆甾相液晶电流体动力 不稳定性的理论研究*

于天池

(郑州工学院数理力学系)

摘要: 本文对负性胆甾相液晶电流体动力不稳定性作了进一步的理论研究。在理论基础上,我们分别考虑了由于边界条件引起的螺距变化以及由于电场作用引起的螺距变化,从而得到了新的修正理论公式。该公式普遍地反映了由于外界条件以及电场感应的螺距变化对于阈值电压的影响,而 Zwart 和 Hurault 理论公式仅是上述公式的两种特殊情况。

关键词: 胆甾相液晶; 阈值; 胆甾平面

中图分类号: O734

我们对负性胆甾相液晶电流体动力不稳定性进行了较系统的实验研究^(1, 2, 3),并在此基础上,利用 Zwart 理论对该实验现象作了初步的理论分析⁽⁴⁾。本文我们将在 Zwart 理论基础上,采用新的物理模型,对此作进一步的理论研究。

1 修正理论公式的建立

如图 1,我们选择一右手直角坐标系 (x, y, z)。假设液晶盒经过表面处理,注入负性胆甾相液晶,使其沿面排列。

设液晶盒厚度为 d,自然螺距为 p₀,考虑到边界条件的影响,实际螺距为 p。

在无外场作用下,未扰动层扭曲角为:

$$\theta = \frac{2\pi}{p} z = mz \quad (1)$$

对于未扰动层,胆甾平面 z 仅是 θ 的函数,即:

$$z(\theta) = \frac{\theta}{m} \quad (2)$$

设沿螺旋轴方向施加一电场:

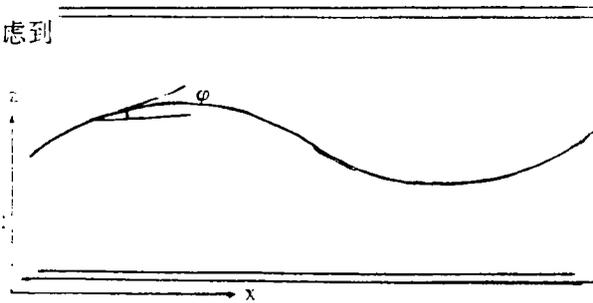


图 1 胆甾平面的周期起伏

* 收稿日期: 1994-12-22

$$E = E_0 \cos \omega t \quad (3)$$

当不稳定性发生后, 胆甾平面沿 x 方向发生周期性形变, 且有:

$$\lambda = 2\pi / K$$

我们假设: $p \ll \lambda \ll d$

$$\text{即: } m \gg K \gg q$$

考虑到在外场作用下螺距的改变, 这时扰动层位置为:

$$z = \frac{\theta}{m} + u_0 + u_1 \quad (4)$$

其中: $u_0 = \frac{p' - p}{p} z$ 是由于外场引起螺距变化产生的位移, p' 是感应平面结构的螺距。

$$u_1 = b \sin qz \cos Kx \quad \text{是微扰}$$

$$b \ll 1, q = \lambda / d$$

这时扭曲角是 x, z 的函数, 且有:

$$\begin{aligned} \theta(x, z) &= \frac{(2p - p')}{p} mz - b \sin qz \cos Kx \\ &= m'z - b \sin qz \cos Kx \\ &= \theta_0 + \alpha \end{aligned} \quad (5)$$

$$\text{而: } m' = \frac{(2p - p')}{p} m$$

$$\theta_0 = m'z \quad (6)$$

$$\alpha = -b \sin qz \cos Kx$$

设弯曲角为:

$$\varphi = \frac{\partial z}{\partial x} = -bK \left(\frac{p}{2p - p'} \right) \sin qz \sin Kx \quad (7)$$

$$= \alpha' \sin qz \sin Kx$$

$$\alpha' = -Kb \left(\frac{p}{2p - p'} \right) \quad (8)$$

α 为扭曲角、 φ 为弯曲角, 它们都是微量, 在扰动情况下, 指向矢方程为:

$$n_x = \cos \theta = \cos \theta_0 - \alpha \sin \theta_0$$

$$n_y = \sin \theta = \sin \theta_0 + \alpha \cos \theta_0 \quad n_z = \varphi(x, z) \cos \theta \quad (9)$$

根据自由能密度公式:

$$g_1 = \frac{1}{2} K_{11} (\nabla \cdot \pi)^2 + \frac{1}{2} K_{22} (\pi \cdot \nabla n \pi + m_0)^2 + \frac{1}{2} K_{33} (\pi_x \nabla_x \pi)^2 \quad (10)$$

$$m_0 = 2\pi / p_0$$

把 (9) 代入 (10) 有:

$$\overline{g_1} = \frac{1}{2} K_{22} \left\{ (m' - m_0)^2 + 2(m' - m_0) \frac{\partial \alpha}{\partial z} + \left(\frac{\partial \alpha}{\partial z} \right)^2 - 2(m' - m_0) \varphi \frac{\partial \alpha}{\partial x} - 2\varphi \frac{\partial \alpha}{\partial x} \frac{\partial \alpha}{\partial z} \right\}$$

$$\begin{aligned}
& + \left(\frac{\partial\varphi}{\partial x}\right)^2 \left[\frac{1}{8}(1-\alpha^2)^2 + \frac{\alpha^2}{2}\right] + \varphi^2 \left(\frac{\partial\alpha}{\partial x}\right)^2 + \frac{1}{2}K_{33} \left\{ \frac{1}{2}(1+\alpha^2) \left[\left(\frac{\partial\alpha}{\partial x}\right)^2 \right. \right. \\
& \left. \left. + 2\varphi(m' + \frac{\partial\alpha}{\partial z})\frac{\partial\alpha}{\partial x} + \varphi^2(m' + \frac{\partial\alpha}{\partial z})^2\right] + \frac{1}{8}\left(\frac{\partial\varphi}{\partial x}\right)^2 [3 + 6\alpha^2 + 3\alpha^4] \right\} \quad (11)
\end{aligned}$$

由于 $\lambda \gg d$, 因此, 上式中略去了 K_{11} 项.

由 $\frac{\partial \bar{g}_1}{\partial K} = 0$ 得:

$$K^2 = qm' \left\{ \frac{8K_{22}}{K_{22} + 3K_{33}} \right\}^{\frac{1}{2}} \quad (12)$$

从自由能密度公式出发, 根据液晶流体动力学方程可得到:

$$\begin{aligned}
\tau_\alpha &= \frac{\alpha}{4}K_{22}\left(\frac{\partial\varphi}{\partial x}\right)^2 + \frac{\alpha}{2}K_{33}\left[\frac{3}{2}\left(\frac{\partial\varphi}{\partial x}\right)^2 + \left(\frac{\partial\alpha}{\partial x}\right)^2 + 2\varphi m'\frac{\partial\alpha}{\partial x} + \varphi^2 m'^2\right] \\
& + K_{22}[(m' - m_0)\frac{\partial\varphi}{\partial x} + \frac{\partial\varphi}{\partial z}\frac{\partial\varphi}{\partial x} + \varphi\frac{\partial}{\partial x}\frac{\partial\alpha}{\partial z} - \varphi^2\frac{\partial^2\alpha}{\partial x^2} - 2\varphi\frac{\partial\varphi}{\partial x}\frac{\partial\alpha}{\partial x}] \\
& - \frac{1}{2}K_{33}\left[\frac{\partial^2\alpha}{\partial x^2} + (m' + \frac{\partial\alpha}{\partial z})\frac{\partial\varphi}{\partial x} + \varphi\frac{\partial}{\partial x}\frac{\partial\alpha}{\partial z} + 2\alpha\left(\frac{\partial\alpha}{\partial x}\right)^2 + \alpha^2\frac{\partial^2\alpha}{\partial x^2}\right] \\
& + m'(2\alpha\varphi\frac{\partial\alpha}{\partial x} + \alpha^2\frac{\partial\varphi}{\partial x}) - K_{22}\left[\frac{\partial^2\alpha}{\partial z^2} - \frac{\partial\varphi}{\partial z}\frac{\partial\alpha}{\partial x} - \varphi\frac{\partial}{\partial z}\frac{\partial\alpha}{\partial x}\right] \\
& - \frac{1}{2}K_{33}\left[\frac{\partial\varphi}{\partial z}\frac{\partial\alpha}{\partial x} + \varphi\frac{\partial}{\partial z}\frac{\partial\alpha}{\partial x} + 2\varphi m'\frac{\partial\varphi}{\partial z} + 2\varphi\frac{\partial}{\partial z}\frac{\partial\alpha}{\partial z} + \varphi^2\frac{\partial^2\alpha}{\partial z^2}\right] \quad (13)
\end{aligned}$$

$$\begin{aligned}
Z_\varphi &= K_{22}\left[\varphi\left(\frac{\partial\alpha}{\partial x}\right)^2 - (m' - m_0)\frac{\partial\alpha}{\partial x} - \frac{\partial\alpha}{\partial x}\frac{\partial\alpha}{\partial z}\right] + \frac{1}{2}K_{33}\left[\frac{\partial\alpha}{\partial x}\frac{\partial\alpha}{\partial z} + m'\frac{\partial\alpha}{\partial x}\right. \\
& \left. + \varphi m'^2 + 2m'\varphi\frac{\partial\alpha}{\partial z} + \varphi\left(\frac{\partial\alpha}{\partial z}\right)^2 + \alpha^2 m'\frac{\partial\alpha}{\partial x} + \alpha^2 m'^2\varphi\right] - \frac{1}{2}K_{22} \\
& \left[\frac{1}{4}\frac{\partial^2\varphi}{\partial x^2} + \frac{1}{2}\alpha^2\frac{\partial^2\varphi}{\partial x^2} + \alpha\frac{\partial\varphi}{\partial x}\frac{\partial\alpha}{\partial x}\right] - \frac{1}{2}K_{33}\left[\frac{3}{4}\frac{\partial^2\varphi}{\partial x^2} + \frac{3}{2}\alpha^2\frac{\partial^2\varphi}{\partial x^2} + 3\alpha\frac{\partial\alpha}{\partial x}\frac{\partial\varphi}{\partial x}\right] \quad (14)
\end{aligned}$$

τ_α 、 τ_φ 分别为扭曲转矩和弯曲转矩

$$\frac{1}{2}(\gamma_1 - \gamma_2)\frac{\partial V_z}{\partial x} - \frac{\epsilon a}{8\pi}(EE_x + E^2\varphi) + Z_\varphi = 0 \quad (15)$$

$$\gamma_1 m' V_z + \tau_\alpha = 0 \quad (16)$$

$$\frac{\partial q}{\partial t} + \frac{q}{\tau} + \sigma_H E \frac{\partial\varphi}{\partial x} = 0 \quad (17)$$

$$\gamma_1 m'^2 V_z = qE \quad (18)$$

$$\text{设: } V_z = V \cos qz \cos Kx \quad (19)$$

$$q = Q(t) \sin qz \cos Kx \quad (20)$$

将相关参数的表达式代入(15)~(18)式中, 联立解得到如下理论公式:

$$V_{th}^2 = \frac{8\pi^3(\epsilon_{11} + \epsilon_{\perp})(1 - w^2\tau^2)}{\epsilon_{\perp}(\epsilon_{\perp} - \epsilon_{11})(\xi - 1 - w^2\tau^2)} K_{22} \left\{ \left(\frac{1}{2} + \frac{3K_{33}}{2K_{22}} \right)^2 + 4 \left(\frac{2p - p'}{p^2} - \frac{1}{p_0} \right) d \right\} \frac{d}{p'} \quad (21)$$

由 (21) 式有:

当 $p' = p \neq p_0$ 时, (21) 式与 Zwart 理论公式一致^[4]

当 $p' = p = p_0$ 时, (21) 式化简为 Hurault 理论公式^[5].

2 实验结果与理论公式的比较

2.1 平行盒情况

我们利用已知液晶材料的物理参数以及实验测量结果, 分别给出了大负性、小负性胆甾相液晶理论曲线及实验点如图 2. 其中 L 和 S 线分别为大负性和小负性的理论曲线, 圆圈和园点分别表示它们的实验值, 实验结果与理论公式基本吻合.

2.2 斜劈盒情况

斜劈盒理论曲线如图 3 所示, 同时我们测得斜劈直条纹宽边, 中间、窄边的实验值. 他们分别用三角、园点和园圈表示. 图中虚线为 Hurault 理论曲线, 它与修正理论公式的理论曲线基本一致.

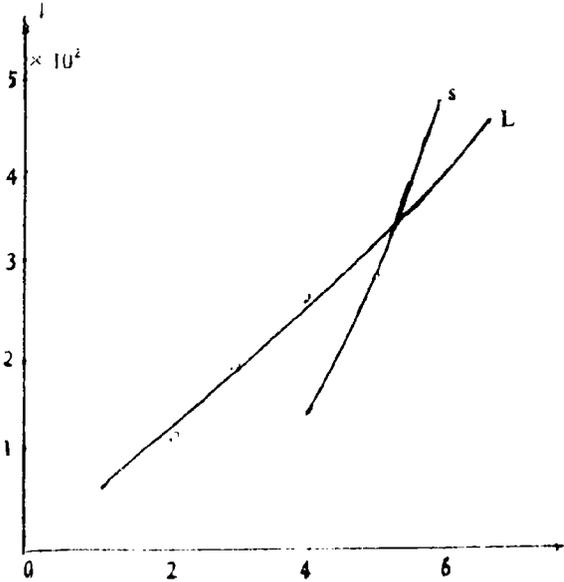


图 2 平行盒阈值电压与螺距数关系曲线

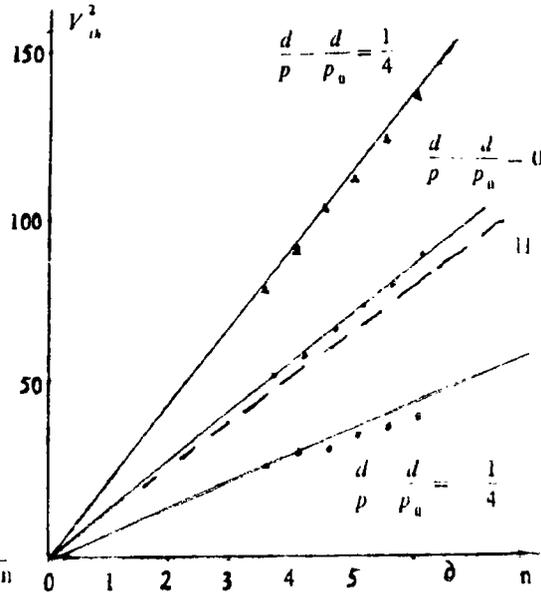


图 3 斜劈盒阈值电压与螺距数关系曲线

以上实验结果与理论公式相比较, 误差在 15% 以内, 新的修正理论公式更普遍地反映了由于外界条件以及电场感应的螺距变化对阈值电压的影响, 而 Zwart 理论和 Hurault 理论仅是上述公式所包含的两种特殊情况.

参 考 文 献

- 1—4 本人论文(待发表)
5 J.P.Huranlt, J.Chem. Phys. 59, 2068(1973)

Investigation of Electrohydrodynamic Instability in Cholesteric Liquid Crystals with Negative Dielectric Anisotropy

Yu Tianchi

(Zhengzhou Institute of Technology)

Abstract: In this paper, On the basis of Zwart's model, We considered the influence of both electric field and boundary condition on pitch, got a new theoretical formula. It described the influence of boundary condition and electric field on threshold voltage, but Zwart's and Huranlt's theoretical formula are only two special example above formula.

Keywords: cholesteric liquid crystals, threshold, cholesteric phanar layer